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# Reliability Estimation in Multi-Component Stress-Strength Based on Burr-III Distribution

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## Abstract

In this paper, we estimate the multicomponent S out of K stress-strength system reliability for Burr-III distribution with non-identical component strengths which are subjected to a common stress. Both stress and strength are assumed to have Burr-III distribution with common and known scale parameter. The research methodology adopted here is to estimate the parameters by using five method of estimation maximum likelihood, least square, weighted least square, regression and moment estimation. The reliability is estimated using the same methods of estimation and results are compared by Monte-Carlo simulation study using MSE and MAPE criteria, the results show that the MI was the best between them.

Keywords: Burr-III distribution, stress-strength, reliability estimation, ML, LS, WLS, Rg and MOM estimation.

## 1. Introduction

Burr 1942 has suggested this family of distributions by solving the following differential equation:-

$$\frac{dy}{dx} = y(1-y)g(x,y), \quad y = F(x),$$

Where the function g(x, y) > 0 must be positive for  $0 \le y \le 1$ , x in the range over which the solution is being satisfied by using different forms of g(x, y) and Pearson systems, Burr in 1941 obtained twelve distribution functions this system is useful for approximating histograms, particularly.[Rodriguez (2004)]

Many researchers studied the Burr-III distribution, like Nahed A. Mokhlis (2005) and Chansoo Kim and Woosuk Kim (2014) (see Kim & Kim (2014) and Mokhlis (2005)).

The CDF of Br3( $\alpha$ ,  $\theta$ ) is:-

$$F(x) = (1 + x^{-\theta})^{-\alpha};$$
  $x > 0; \ \alpha, \theta > 0$  (1)

Where the parameters  $\theta > 0$  and  $\alpha > 0$  are the shape parameters of the distribution. Its PDF is:-

$$f(x) = \alpha \theta x^{-(\theta+1)} (1 + x^{-\theta})^{-(\alpha+1)}; \qquad x > 0; \ \alpha, \theta > 0$$
(2)

The stress-strength model is used in many applications in physics and engineering. In the statistical approach to the stress-strength model, most of the considerations depend on the assumption that the component strengths are independently and identically distributed (iid) and are subjected to a common stress. [Hassan & Basheikh  $(2012)^1$ ]

The system reliability of multicomponent based on X and Y two independent and identical random variable.

The system of multicomponent stress-strength studied by Amal S. Hassan and Heba M. Basheikh (2012) [Hassan & Basheikh  $(2012)^2$ ] where they expanded the system of multicomponent to be with 2-part multicomponent stress-strength.

The main aim of this article is to discuss the derivation of the mathematical formula of reliability in multicomponent stress-strength  $R_{s,k}$  for Burr type III distribution, then estimation  $R_{s,k}$  by using ML, LS, WLS, Rg and MOM methods, and comparison among the results of the estimation methods by using mean square error (MSE) and mean absolute percentage error (MAPE), that will get from a simulation study.

#### 2. Experimental Aspect of Reliability in multicomponent stress-strength:-

In this article, the system made up of k non-identical components. Out of these k components,  $k_1$  are of one category and their strengths  $Y_1, Y_2, ..., Y_{k_1}$  are iid random variables distributed Br3D with parameters  $(\alpha_1, \theta)$ . The remaining components  $k_2 = k - k_1$  are of different category and their strengths  $Y_{k_1+1}, Y_{k_1+2}, ..., Y_k$  are iid

random variables distributed Br3D with parameters  $(\alpha_2, \theta)$ . This system is subjected to a common stress *X* which is independent random variable distributed Br3D with parameters  $(\lambda, \theta)$ . Let  $f_1(y_1; \alpha_1, \theta)$  be a common probability density function (PDF) of strengths  $Y_1, Y_2, ..., Y_{k_1}, f_2(y_2; \alpha_2, \theta)$  be a common PDF of strengths  $Y_{k_1+1}, Y_{k_1+2}, ..., Y_k$  and  $g(x; \lambda, \theta)$  be PDF of stress *X*. The corresponding cumulative distribution functions are given, respectively, by: [Hassan & Basheikh (2012)<sup>2</sup>]

$$F_{1}(y_{1}; \alpha_{1}, \theta) = (1 + y_{1}^{-\theta})^{-\alpha_{1}}; \qquad y_{1} > 0; \ \alpha_{1} \ and \ \theta > 0,$$

$$F_{2}(y_{2}; \alpha_{2}, \theta) = (1 + y_{2}^{-\theta})^{-\alpha_{2}}; \qquad y_{2} > 0; \ \alpha_{2} \ and \ \theta > 0,$$

$$G(x; \lambda, \theta) = (1 + y^{-\theta})^{-\lambda}; \qquad y > 0; \ \lambda \ and \ \theta > 0.$$
(3)

The system operates successfully, if at least *s* out of *k* components withstand the stress. According to Johnson, the system reliability with non-identical component strengths  $R_{(s,k)}$  is given by

$$R_{(s,k)} = \sum_{i_1=s_1}^{k_1} C_{i_1}^{k_1} \sum_{i_2=s_2}^{k_2} C_{i_2}^{k_2} \int_0^\infty [1 - F_1(x)]^{i_1} [F_1(x)]^{k_1 - i_1} [1 - F_2(x)]^{i_2} [F_2(x)]^{k_2 - i_2} dG(X)$$
(4)

Where the summation is over all possible pair  $(i_1, i_2)$  with  $0 \le i_1 \le k_1$  and  $0 \le i_2 \le k_2$  such that  $s \le i_1 + i_2 \le k$ . It is important to note that the system reliability can be extended to more than two groups of components. The reliability of *s*-out-of-*k* system for Br3 can be computed by substituting equations (3) in equation (4) and simplifying:

$$R_{(s,k)} = \sum_{i_1=s_1}^{k_1} C_{i_1}^{k_1} \sum_{i_2=s_2}^{k_2} C_{i_2}^{k_2} \int_0^\infty [1 - (1 + y^{-\theta})^{-\alpha_1}]^{i_1} [(1 + y^{-\theta})^{-\alpha_1}]^{k_1 - i_1} [1 - (1 + y^{-\theta})^{-\alpha_2}]^{i_2} [(1 + y^{-\theta})^{-\alpha_2}]^{k_2 - i_2} \lambda \theta y^{-(\theta + 1)} (1 + y^{-\theta})^{-(\lambda + 1)} dy$$

$$R_{(s,k)} = \lambda \sum_{i_1=s_1}^{k_1} C_{i_1}^{k_1} \sum_{i_2=s_2}^{k_2} C_{i_2}^{k_2} \sum_{j_1=0}^{i_1} C_{j_1}^{i_1} (-1)^{j_1} \sum_{j_2=0}^{i_2} C_{j_2}^{i_2} (-1)^{j_2} \int_0^1 u^{[\alpha_1(j+k_1-i_1)+\alpha_2(j_2+k_2-i_2)+\lambda+1]} du \text{ where } u = (1+y^{-\theta})^{-1}$$

Then the  $R_{(s,k)}$  of Br3D is given by:-

$$R_{(s,k)} = \lambda \sum_{i_1=s_1}^{k_1} C_{i_1}^{k_1} \sum_{i_2=s_2}^{k_2} C_{i_2}^{k_2} \sum_{j_1=0}^{i_1} C_{j_1}^{i_1} (-1)^{j_1} \sum_{j_2=0}^{i_2} C_{j_2}^{i_2} (-1)^{j_2} [\alpha_1(j_1+k_1-i_1)+\alpha_2(j_2+k_2-i_2)+\lambda]^{-1}$$
(5)

Where i, s, k and j are integers.

#### 3. Different method of estimation:

The unknown shape parameters of  $R_{(s,k)}$  for Br3D have been estimated by five methods of estimation; ML, LS, WLS, Rg and MOM.

## 3.1 Maximum likelihood function (MLE):-

Let  $X_{1_{i_1}}$ ;  $i_1 = 1, 2, ..., n_1$  and  $X_{2_{i_2}}$ ;  $i_2 = 1, 2, ..., n_2$  strength random samples from  $Br3(\alpha_1, \theta)$  and  $Br3(\alpha_2, \theta)$  with sample size  $n_1$  and  $n_2$ , respectively, where  $\alpha_1$  and  $\alpha_2$  are unknown parameters, and let Y stress random variable with sample size *m* is drawn from  $Br3(\lambda, \theta)$  where  $\lambda$  is unknown parameter. Then the likelihood function *L*, using equation (2) as:-[Shawky and AL-Kashkari (2007)]

$$L\left(x_{1}, x_{2}, \dots, x_{n_{\xi}}; \alpha_{\xi}, \theta\right) = \prod_{i_{\xi}=1}^{n_{\xi}} \left[ \alpha_{\xi} \theta x_{\xi_{i_{\xi}}}^{-(\theta+1)} \left( 1 + x_{\xi_{i_{\xi}}}^{-\theta} \right)^{-(\alpha_{\xi}+1)} \right]$$

And 
$$L(y; \lambda, \theta) = \prod_{j=1}^{m} \left[ \lambda \theta y_j^{-(\theta+1)} \left( 1 + y_j^{-\theta} \right)^{-(\lambda+1)} \right]$$
; where ;  $\xi = 1, 2$ 

The partial derivative of log-likelihood function with respect to  $\alpha_{\xi}$  and  $\lambda$  are given by:

Then by simplification equations (6), the ML's estimator for the unknown shape parameters  $\alpha_{\xi}$  and  $\lambda$ ,  $(\hat{\alpha}_{\xi^{MLE}}, \hat{\lambda}_{MLE})$  for  $R_{(s,k)}$ , are:

$$\hat{\alpha}_{\xi^{MLE}} = \frac{n_{\xi}}{\sum_{i_{\xi}=1}^{n_{\xi}} ln\left(1 + x_{\xi_{i_{\xi}}}^{-\theta}\right)}, \xi = 1, 2; \ \hat{\lambda}_{MLE} = \frac{m}{\sum_{j=1}^{m} ln(1 + y_{j}^{-\theta})}$$
(7)

Substation the equations (7) in the equations (5), the ML estimator for  $R_{(s,k)}$ ,  $(\hat{R}_{BML})$ , can be obtained as:

$$\hat{R}_{BML} = \hat{\lambda}_{MLE} \sum_{i_1=s_1}^{k_1} \sum_{i_2=s_2}^{k_2} C_{i_1}^{k_1} C_{i_2}^{k_2} \sum_{j_1=0}^{i_1} C_{j_1}^{i_1} (-1)^{j_1} \sum_{j_2=0}^{i_2} C_{j_2}^{i_2} (-1)^{j_2} \\ \left[ \hat{\alpha}_{1^{MLE}}(j_1 + k_1 - i_1) + \hat{\alpha}_{2^{MLE}}(j_2 + k_2 - i_2) + \lambda_{MLE} \right]^{-1}$$

## 3.2 Least Square Method (LS):-

The method of least square is very popular for model fitting, especially in linear and non-linear regression, it can be produce by minimizing the sum of square error between the value and it's expected value. [Ali (2013)]

$$s_{1} = \sum_{i_{\xi}=1}^{n_{\xi}} \left[ F(x_{(i_{\xi})}) - E\left(F\left(x_{(i_{\xi})}\right)\right) \right]^{2} S = \sum_{i=1}^{n} \left[ F(y_{(i)}) - E\left(F(y_{(i)})\right) \right]^{2}$$
(8)

Where  $E\left(F\left(x_{(i_{\xi})}\right)\right)$  and  $E\left(F(y_{(i)})\right)$  equal to  $P_{i_{\xi}}$ ,  $P_{j}$  the plotting position, where

$$P_{i\xi} = \frac{i_{\xi}}{n_1 + 1}, i_{\xi} = 1, 2, \dots, n_{\xi} \text{ and } \xi = 1, 2, \text{ and } P_j = \frac{j}{m + 1} \text{and} i = 1, 2, \dots, m.$$
(9)

We obtain the LS estimators to the unknown shape parameters  $\alpha_1, \alpha_2$  to the strength r.v.'s  $X_1 \sim Br3(\alpha_1, \theta)$ ,  $X_2 \sim Br3(\alpha_2, \theta)$  with sample size  $n_1$  and  $n_2$ , respectively, and  $\lambda$  to the stress r.v.  $Y \sim Br3(\lambda, \theta)$  with sample size m. From a distribution function (1), simplification and changing  $F(x_{\xi_{(i_{\xi})}}), G(y_{(j)})$  by plotting position  $P_{i_{\xi}}, P_j$  (9), and equal to zero, we obtain:-

$$\ln \left(P_{i\xi}\right)^{-1} - \alpha_{\xi} \ln \left(1 + x_{\xi_{(i\xi)}}^{-\theta}\right) = 0; \ \xi = 1,2$$

$$\ln \left(P_{j}\right)^{-1} - \lambda \ln \left(1 + y_{(j)}^{-\theta}\right) = 0$$
(10)

Substitution (10) in (8) and taking the first derivative with respect to the unknown shape parameters  $\alpha_{\xi}$  and  $\lambda$ , and equating the result to zero, we get:

$$\hat{\alpha}_{\xi LS} = \frac{\sum_{i_{\xi}=1}^{n_{\xi}} \left( \ln\left(P_{i_{\xi}}\right)^{-1} \ln\left(1 + x_{\xi(i_{\xi})}^{-\theta}\right) \right)}{\sum_{i_{\xi}=1}^{n_{\xi}} \left( \ln\left(1 + x_{\xi(i_{\xi})}^{-\theta}\right) \right)^{2}}, \xi = 1, 2$$

$$\hat{\lambda}_{LS} = \frac{\sum_{j=1}^{n} \left( \ln\left(P_{j}\right)^{-1} \ln\left(1 + y_{(j)}^{-\theta}\right) \right)}{\sum_{j=1}^{n} \left( \ln\left(1 + y_{(j)}^{-\theta}\right) \right)^{2}}$$
(11)

Where  $P_{i\xi}$  and  $P_j$  as in (9).

Substitution the equations (11) in the equation (5), the LS estimator for  $R_{(s,k)}$ ,  $(\hat{R}_{BLS})$ , approximately can be obtained as:

$$\begin{aligned} \hat{R}_{BLS} &= \hat{\lambda}_{LS} \sum_{i_1=s_1}^{k_1} \sum_{i_2=s_2}^{k_2} C_{i_1}^{k_1} C_{i_2}^{k_2} \sum_{j_1=0}^{i_1} C_{j_1}^{i_1} (-1)^{j_1} \sum_{j_2=0}^{i_2} C_{j_2}^{i_2} (-1)^{j_2} \\ & \left[ \hat{\alpha}_{1^{LS}}(j_1 + k_1 - i_1) + \hat{\alpha}_{2^{LS}}(j_2 + k_2 - i_2) + \hat{\lambda}_{LS} \right]^{-1} \end{aligned}$$

#### 3.3 Weighted Least Square Method (WLS):-

The estimators weighted least squares can be obtained by minimizing the following equation.[Ali (2013)]

$$s_{1} = \sum_{i_{\xi}=1}^{n_{\xi}} \omega_{i_{\xi}} \left[ F(x_{(i_{\xi})}) - E\left(F\left(x_{(i_{\xi})}\right)\right) \right]^{2} \text{ and } s_{2} = \sum_{j=1}^{m} \omega_{j} \left[F(y_{(j)}) - E\left(F(y_{(i)})\right)\right]^{2}$$
(12)

With respect to the unknown parameters  $\alpha_{\xi}$  and  $\lambda$ , Where  $E\left(F\left(x_{(i_{\xi})}\right)\right)$  and  $E(F(y_{(i)}))$  equal to  $P_{i_{\xi}}$ ,  $P_{j}$  the plotting position, where  $P_{i_{\xi}}$ ,  $P_{j}$  as in (9)

And 
$$\omega_{i_{\xi}} = \frac{1}{Var\left[F\left(x_{\xi(i_{\xi})}\right)\right]} = \frac{(n_{\xi}+1)^{2}(n_{\xi}+2)}{i_{\xi}(n_{\xi}-i+1)}, i_{\xi} = 1, 2, ..., n_{\xi}$$
  
and  $\omega_{j} = \frac{1}{Var[G\left(y_{(j)}\right)]} = \frac{(m+1)^{2}(m+2)}{j(m-j+1)}, j = 1, 2, ..., m$ 

$$(13)$$

We obtain the WLS estimators to the unknown shape parameters  $\alpha_1, \alpha_2$  to the strength r.v.'s  $X_1 \sim Br3(\alpha_1, \theta)$ ,  $X_2 \sim Br3(\alpha_2, \theta)$  with sample size  $n_1$  and  $n_2$ , respectively, and  $\lambda$  to the stress r.v.  $Y \sim Br3(\lambda, \theta)$  with sample size m, by substitution (10) in (12), and taking the partial derivative with respect to the unknown shape parameters  $\alpha_{\xi}$  and  $\lambda$ , and simplify the result, then the final formulas can be written as:

$$\hat{\alpha}_{\xi} w_{LS} = \frac{\sum_{i_{\xi}=1}^{n_{\xi}} \omega_{i_{\xi}} \left( \ln \left( P_{i_{\xi}} \right)^{-1} \ln \left( 1 + x_{\xi} \right)^{-\theta} \right) \right)}{\sum_{i_{\xi}=1}^{n_{\xi}} \omega_{i_{\xi}} \left( \ln \left( 1 + x_{\xi} \right)^{-\theta} \right) \right)^{2}}, \xi = 1, 2$$

$$\hat{\lambda}_{WLS} = \frac{\sum_{j=1}^{n} \omega_{j} \left( \ln \left( P_{j} \right)^{-1} \ln \left( 1 + y_{(j)} \right)^{-\theta} \right) \right)}{\sum_{j=1}^{n} \omega_{j} \left( \ln \left( 1 + y_{(j)} \right)^{-\theta} \right) \right)^{2}}$$
(14)

Where the plotting position  $P_{i\xi}$  and  $P_{j}$  as in (9), and  $\omega_{i\xi}$  and  $\omega_{j}$  as in (13).

Substitution the equations (14) in the equation (5), the WLS estimator for  $R_{(s,k)}$ ,  $(\hat{R}_{BWL})$ , can be obtained as:

$$\hat{R}_{BWL} = \hat{\lambda}_{WLS} \sum_{i_1=s_1}^{k_1} \sum_{i_2=s_2}^{k_2} C_{i_1}^{k_1} C_{i_2}^{k_2} \sum_{j_1=0}^{i_1} C_{j_1}^{i_1} (-1)^{j_1} \sum_{j_2=0}^{i_2} C_{j_2}^{i_2} (-1)^{j_2}$$

$$[\hat{\alpha}_{1} W LS(j_{1} + k_{1} - i_{1}) + \hat{\alpha}_{2} W LS(j_{2} + k_{2} - i_{2}) + \hat{\lambda}_{W LS}]^{-1}$$

## 3.4 Regression Method (Rg):-

Regression is one of the important procedures that use auxiliary information to construct estimators with good efficiency. [Park (2012)]

The standard regression equation:-

,

$$z_i = a + bu_i + e_i \tag{15}$$

Where  $z_i$  is dependent variable (response variable),  $u_i$  is independent variable (Explanatory Variable) and  $e_i$  is the error r.v. independent identically Normal distributed with  $(0, \sigma^2)$ .

Taking natural logarithm to (1), then changing  $F(x_{(i)})$  and  $G(y_{(j)})$  by plotting position  $P_{i\xi}$  and  $P_j$  (9), then simplification the result, we obtain:

Comparing the equation (16) with the equation (15), we get:

$$z_{i} = \ln P_{i_{\xi}}, a = 0, b = \alpha_{\xi}, u_{i} = -\ln\left(1 + x_{\xi_{(i_{\xi})}}^{-\theta}\right)$$

$$z_{i} = \ln P_{j}, a = 0, b = \lambda, u_{i} = -\ln(1 + y_{(j)}^{-\theta})$$
(17)

Where b can be estimated by minimizing the summation of squared error with respect to b, then we get:

$$\hat{b} = \frac{n\sum_{i=1}^{n} z_{i}u_{i} - \sum_{i=1}^{n} z_{i}\sum_{i=1}^{n} u_{i}}{n\sum_{i=1}^{n} (u_{i})^{2} - \left[\sum_{i=1}^{n} u_{i}\right]^{2}}$$
(18)

And by substitution (17) in (18) we obtain the estimate for unknown shape parameters  $\alpha_{\xi}$  and  $\lambda$  for  $R_{s,k}$  then the result will be:

$$\hat{\alpha}_{\xi^{Rg}} = \frac{n_{\xi} \sum_{i_{\xi}=1}^{n_{\xi}} \ln P_{i_{\xi}} \ln \left(1 + x_{\xi(i_{\xi})}^{-\theta}\right) - \sum_{i_{\xi}=1}^{n_{\xi}} \ln P_{i_{\xi}} \sum_{i_{\xi}=1}^{n_{\xi}} \ln \left(1 + x_{\xi(i_{\xi})}^{-\theta}\right)}{n_{\xi} \sum_{i_{\xi}=1}^{n_{\xi}} \left[\ln \left(1 + x_{\xi(i_{\xi})}^{-\theta}\right)\right]^{2} - \left[\sum_{i_{\xi}=1}^{n_{\xi}} \ln \left(1 + x_{\xi(i_{\xi})}^{-\theta}\right)\right]^{2}}; \text{ Where } \xi = 1,2$$

$$\hat{\lambda}_{Rg} = \frac{m \sum_{j=1}^{m} \ln P_{j} \ln (1 + y_{(j)}^{-\theta}) - \sum_{j=1}^{m} \ln P_{j} \sum_{j=1}^{m} \ln (1 + y_{(j)}^{-\theta})}{m \sum_{j=1}^{m} \left[\ln (1 + y_{(j)}^{-\theta})\right]^{2} - \left[\sum_{j=1}^{m} \ln (1 + y_{(j)}^{-\theta})\right]^{2}}$$

$$(19)$$

Where the plotting position  $P_{i_{\xi}}$  and  $P_j$  as in (9).

Substitution the equations (19) in the equation (5), the RM estimator for  $R_{(s,k)}$ ,  $(\hat{R}_{BRg})$ , can be obtained as:  $\hat{R}_{BRg} = \hat{\lambda}_{Rg} \sum_{i_1=s_1}^{k_1} \sum_{i_2=s_2}^{k_2} C_{i_1}^{k_1} C_{i_2}^{k_2} \sum_{j_1=0}^{i_1} C_{j_1}^{i_1} (-1)^{j_1} \sum_{j_2=0}^{i_2} C_{j_2}^{i_2} (-1)^{j_2}$ 

$$\left[\hat{\alpha}_{1^{Rg}}(j_1+k_1-i_1)+\hat{\alpha}_{2^{Rg}}(j_2+k_2-i_2)+\lambda_{Rg}\right]^{-1}$$

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#### 3.5 Moment method (MOM):-

The MOM was one of the first methods used to estimate the society parameter  $\theta$ , it was introduced by Pearson (1894). [Ali (2013)]

To derive the method of moment estimators of the parameters of a Br3D, let  $X_{1_{i_1}}$ ;  $i_1 = 1, 2, ..., n_1$  and  $X_{2_{i_2}}$ ;  $i_2 = 1, 2, ..., n_2$  strength random samples from  $Br3(\alpha_1, \theta)$  and  $Br3(\alpha_2, \theta)$  with sample size  $n_1$  and  $n_2$ , respectively, where  $\alpha_1$  and  $\alpha_2$  are unknown parameters, and let Y stress random variable with sample size m is drawn from  $Br3(\lambda, \theta)$  where  $\lambda$  is unknown parameter, , we need the population mean:

$$E(x_{\xi}) = \alpha_{\xi} B\left(1 - \frac{1}{\theta}, \alpha_{\xi} + \frac{1}{\theta}\right); \text{ where } \theta > 2$$
$$E(y) = \lambda B\left(1 - \frac{1}{\theta}, \lambda + \frac{1}{\theta}\right); \text{ where } \theta > 2$$

For  $\theta$  is known, equating the sample mean with corresponding populations mean, we get the shape parameters moment estimators.

$$\frac{\sum_{i_{\xi}=1}^{n_{\xi}} x_{\xi_{i_{\xi}}}}{n_{\xi}} = \alpha_{\xi} B\left(1 - \frac{1}{\theta}, \alpha_{\xi} + \frac{1}{\theta}\right); \qquad \frac{\sum_{j=1}^{m} y_{j}}{m} = \lambda B\left(1 - \frac{1}{\theta}, \lambda + \frac{1}{\theta}\right)$$

By simplification we obtain the estimators to the unknown shape parameters  $\alpha_{\xi}$  and  $\lambda$  for  $R_{(s,k)}$  ( $\hat{\alpha}_{\xi MOM}$  and  $\hat{\lambda}_{MOM}$ ), then the result will be:

$$\hat{\alpha}_{\xi^{MOM}} = \frac{x_{\xi}}{B\left(1 - \frac{1}{\theta}, \alpha_{\xi_0} + \frac{1}{\theta}\right)}; \quad \text{where } \xi = 1, 2; \ \theta > 2$$

$$\hat{\lambda}_{MOM} = \frac{\bar{y}}{B\left(1 - \frac{1}{\theta}, \lambda_0 + \frac{1}{\theta}\right)}; \quad \text{where } \theta > 2$$
(19)

Substitution the equations (19) in the equation (5), the MOM estimator for  $R_{(s,k)}$ ,  $(\hat{R}_{BMOM})$ , can be obtained as:

$$\hat{R}_{BMOM} = \hat{\lambda}_{MOM} \sum_{i_1=s_1}^{k_1} \sum_{i_2=s_2}^{k_2} C_{i_1}^{k_1} C_{i_2}^{k_2} \sum_{j_1=0}^{i_1} C_{j_1}^{i_1} (-1)^{j_1} \sum_{j_2=0}^{i_2} C_{j_2}^{i_2} (-1)^{j_1} C_{j_2}^{i_2} (-1)^{j_2} C_{j_2}^{i_2} (-1)^{j_2$$

$$\left[\hat{\alpha}_{1}^{MOM}(j_{1}+k_{1}-i_{1})+\hat{\alpha}_{2}^{MOM}(j_{2}+k_{2}-i_{2})+\lambda_{MOM}\right]^{T}$$

## 4. Simulation study:

Results based on Monte Carlo simulations to compare the performance of the  $R_{(s,k)}$  using different sample sizes are presented. 1500 random sample of size 10,20,35,50.75 and 100 each from stress population, strength population were generated  $(\alpha_1, \alpha_2, \lambda, \theta) = (1.5, 2, 0.8, 1.2), (\alpha_1, \alpha_2, \lambda, \theta) = (1.5, 2, 2.3, 1.2)$  for  $(s_1, k_1, s_2, k_2) =$ (2, 3, 3, 4) and  $(s_1, k_1, s_2, k_2) = (1, 2, 3, 3)$  for  $R_{(s,k)}$ . The Mean square error (MSE) and Mean Absolute Percentage Error (MAPE) of the reliability estimates over the 1500 replications are given in Tables 2 and 3.

The true value of reliability in multicomponent stress- strength  $R_{(s,k)}$  with the given combinations of  $(\alpha_1, \alpha_2, \lambda, \theta) = (1.5, 2, 0.8, 1.2), (\alpha_1, \alpha_2, \lambda, \theta) = (1.5, 2, 2.3, 1.2)$  for  $(s_1, k_1, s_2, k_2) = (2, 3, 3, 4)$  are  $R_{(s,k)} = 0.5755$  and  $R_{(s,k)} = 0.2411$  and for  $(s_1, k_1, s_2, k_2) = (1, 2, 3, 3)$  are  $R_{(s,k)} = 0.5024$  and  $R_{(s,k)} = 0.1863$ . From the tables (2) and (3) below, we have observed that:-

- 1- When  $(s_1, k_1, s_2, k_2) = (2, 3, 3, 4)$ :-
- the MSE value decreasing by increasing sample size for MLE, LS, WLS, Rg and MOM estimators. The best MSE value is MLE estimator, followed by LS, WLS, Rg and MOM.
- The MAPE value decreasing by increasing sample size for MLE, LS, WLS, Rg and MOM estimators. The best MAPE value is MLE estimator, followed by LS, WLS, Rg and MOM.
- 2- When  $(s_1, k_1, s_2, k_2) = (1, 2, 3, 3)$ :-

- The MSE value decreasing by increasing sample size for MLE, LS, WLS, Rg and MOM estimators. The best MSE value is MLE estimator, followed by LS, WLS, Rg and MOM.
- The MAPE value decreasing by increasing sample size for MLE, LS, WLS, Rg and MOM estimators. The best MAPE value is MLE estimator, followed by LS, WLS, Rg and MOM.

# 5. Conclusion:

- The MSE and MAPE value decreases by increasing sample size.
- The performance MLE was the best, followed by LS, WLS, Rg and MOM for all sample sizes, as in the table below.

**Table (1):** The best estimation method of MSE and MAPE of Br3 for  $R_{(s,k)}$ .

| Method<br>Sample size | MLE | LS | WLS | Rg | МОМ | Best |
|-----------------------|-----|----|-----|----|-----|------|
| All sample size       | 1   | 2  | 3   | 4  | 5   | MLE  |

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| Methods         | $(s_1, k_1, s_2, k_2)$ |              |        |        |        |        |               |          |
|-----------------|------------------------|--------------|--------|--------|--------|--------|---------------|----------|
| $(n_1, n_1, m)$ |                        |              | MLE    | LS     | WLS    | Rg     | MOM           | Best     |
|                 |                        | Mean         | 0.5572 | 0.5528 | 0.5512 | 0.5430 | 0.5285        | _        |
| (10,10,10)      |                        | MSE          | 0.0131 | 0.0154 | 0.0161 | 0.0221 | 0.0535        | MLE      |
|                 | (2, 3, 3, 4)           | MAPE         | 0.1562 | 0.1701 | 0.1741 | 0.2058 | 0.3260        | MLE      |
| (20,20,20)      |                        | Mean         | 0.5635 | 0.5619 | 0.5567 | 0.5568 | 0.5266        | -        |
|                 |                        | MSE          | 0.0068 | 0.0082 | 0.0093 | 0.0122 | 0.0441        | MLE      |
|                 |                        | MAPE         | 0.1127 | 0.1239 | 0.1325 | 0.1531 | 0.2856        | MLE      |
| (35,35,35)      |                        | Mean         | 0.5689 | 0.5680 | 0.5595 | 0.5650 | 0.5287        | -        |
|                 |                        | MSE          | 0.0039 | 0.0048 | 0.0060 | 0.0073 | 0.0377        | MLE      |
|                 |                        | MAPE         | 0.0859 | 0.0965 | 0.1077 | 0.1190 | 0.2606        | MLE      |
|                 | (2, 0, 0, 4)           | Mean         | 0.5727 | 0.5723 | 0.5633 | 0.5701 | 0.5445        | -        |
| (50,50,50)      |                        | MSE          | 0.0027 | 0.0031 | 0.0040 | 0.0048 | 0.0315        | MLE      |
|                 |                        | MAPE         | 0.0726 | 0.0780 | 0.0885 | 0.0961 | 0.2346        | MLE      |
| (75,75,75)      |                        | Mean         | 0.5725 | 0.5724 | 0.5615 | 0.5711 | 0.5471        | -        |
|                 |                        | MSE          | 0.0017 | 0.0022 | 0.0032 | 0.0034 | 0.0258        | MLE      |
|                 |                        | MAPE         | 0.0578 | 0.0646 | 0.0777 | 0.0808 | 0.2081        | MLE      |
| (100,100,100)   |                        | Mean         | 0.5724 | 0.5716 | 0.5600 | 0.5698 | 0.5486        |          |
|                 |                        | MSE          | 0.0012 | 0.0016 | 0.0026 | 0.0026 | 0.0250        | MLE      |
| -               |                        | MAPE<br>Mean | 0.0487 | 0.0552 | 0.0695 | 0.0707 | 0.2054 0.4907 | MLE      |
| (10,10,10)      |                        | MSE          | 0.4940 | 0.4908 | 0.4901 | 0.4848 | 0.4907        | -<br>MLE |
| (10,10,10)      |                        | MAPE         | 0.1950 | 0.2093 | 0.2144 | 0.2470 | 0.3847        | MLE      |
| (20,20,20)      |                        | Mean         | 0.4943 | 0.4940 | 0.4899 | 0.4916 | 0.4773        | -        |
|                 |                        | MSE          | 0.0082 | 0.0097 | 0.0110 | 0.0141 | 0.0461        | MLE      |
|                 |                        | MAPE         | 0.1442 | 0.1566 | 0.1672 | 0.1898 | 0.3498        | MLE      |
| (35,35,35)      |                        | Mean         | 0.5013 | 0.4992 | 0.4912 | 0.4958 | 0.4921        | -        |
|                 | (1, 2, 3, 3)           | MSE          | 0.0049 | 0.0061 | 0.0077 | 0.0090 | 0.0366        | MLE      |
|                 |                        | MAPE         | 0.1117 | 0.1257 | 0.1401 | 0.1528 | 0.3079        | MLE      |
| (50,50,50)      |                        | Mean         | 0.5021 | 0.5024 | 0.4943 | 0.5016 | 0.4856        | -        |
|                 |                        | MSE          | 0.0033 | 0.0040 | 0.0054 | 0.0062 | 0.0346        | MLE      |
|                 |                        | MAPE         | 0.0918 | 0.1014 | 0.1166 | 0.1254 | 0.2915        | MLE      |
| (75,75,75)      |                        | Mean         | 0.5004 | 0.5003 | 0.4902 | 0.4997 | 0.4855        | -        |
|                 |                        | MSE          | 0.0022 | 0.0027 | 0.0040 | 0.0041 | 0.0307        | MLE      |
|                 |                        | MAPE         | 0.0746 | 0.0830 | 0.1000 | 0.1022 | 0.2740        | MLE      |
| (100,100,100)   |                        | Mean         | 0.5010 | 0.5006 | 0.4897 | 0.4998 | 0.4832        | -        |
|                 |                        | MSE          | 0.0017 | 0.0021 | 0.0033 | 0.0033 | 0.0300        | MLE      |
|                 |                        | MAPE         | 0.0661 | 0.0728 | 0.0899 | 0.0905 | 0.2663        | MLE      |

| Methods<br>( <i>n</i> <sub>1</sub> , <i>n</i> <sub>1</sub> , <i>m</i> ) | $(s_1, k_1, s_2, k_2)$ |                     | MLE                        | LS                         | WLS                        | Rg                         | MOM                        | Best            |
|---|------------------------|---------------------|----------------------------|----------------------------|----------------------------|----------------------------|----------------------------|-----------------|
| (10,10,10)  | (2, 3, 3, 4)           | Mean<br>MSE<br>MAPE | 0.2465<br>0.0112<br>0.3551 | 0.2455<br>0.0125<br>0.3717 | 0.2449<br>0.0128<br>0.3775 | 0.2449<br>0.0169<br>0.4305 | 0.2489<br>0.0338<br>0.6234 | -<br>MLE<br>MLE |
| (20,20,20)  |                        | Mean<br>MSE<br>MAPE | 0.2415<br>0.0059<br>0.2554 | 0.2414<br>0.0070<br>0.2812 | 0.2377<br>0.0077<br>0.2953 | 0.2417<br>0.0102<br>0.3372 | 0.2455<br>0.0273<br>0.5575 | -<br>MLE<br>MLE |
| (35,35,35)  |                        | Mean<br>MSE<br>MAPE | 0.2408<br>0.0036<br>0.1975 | 0.2414<br>0.0044<br>0.2214 | 0.2351<br>0.0051<br>0.2404 | 0.2422<br>0.0066<br>0.2709 | 0.2351<br>0.0223<br>0.5055 | -<br>MLE<br>MLE |
| (50,50,50)  |                        | Mean<br>MSE<br>MAPE | 0.2426<br>0.0025<br>0.1685 | 0.2430<br>0.0029<br>0.1807 | 0.2358<br>0.0035<br>0.1986 | 0.2435<br>0.0044<br>0.2210 | 0.2433<br>0.0198<br>0.4672 | -<br>MLE<br>MLE |
| (75,75,75)  |                        | Mean<br>MSE<br>MAPE | 0.2414<br>0.0017<br>0.1389 | 0.2417<br>0.0022<br>0.1557 | 0.2326<br>0.0029<br>0.1798 | 0.2418<br>0.0035<br>0.1942 | 0.2400<br>0.0176<br>0.4482 | -<br>MLE<br>MLE |
| (100,100,100)   |                        | Mean<br>MSE<br>MAPE | 0.2415<br>0.0012<br>0.1147 | 0.2417<br>0.0016<br>0.1333 | 0.2325<br>0.0023<br>0.1616 | 0.2419<br>0.0026<br>0.1697 | 0.2418<br>0.0158<br>0.4182 | -<br>MLE<br>MLE |
| (10,10,10)  | (1, 2, 3, 3)           | Mean<br>MSE<br>MAPE | 0.1954<br>0.0096<br>0.4198 | 0.1973<br>0.0109<br>0.4442 | 0.1973<br>0.0113<br>0.4502 | 0.2016<br>0.0154<br>0.5277 | 0.2177<br>0.0340<br>0.7769 | -<br>MLE<br>MLE |
| (20,20,20)  |                        | Mean<br>MSE<br>MAPE | 0.1874<br>0.0049<br>0.2983 | 0.1882<br>0.0059<br>0.3316 | 0.1861<br>0.0065<br>0.3477 | 0.1911<br>0.0088<br>0.4036 | 0.2128<br>0.0274<br>0.6905 | -<br>MLE<br>MLE |
| (35,35,35)  |                        | Mean<br>MSE<br>MAPE | 0.1904<br>0.0031<br>0.2385 | 0.1905<br>0.0038<br>0.2628 | 0.1860<br>0.0044<br>0.2861 | 0.1919<br>0.0057<br>0.3191 | 0.2125<br>0.0232<br>0.6329 | -<br>MLE<br>MLE |
| (50,50,50)  |                        | Mean<br>MSE<br>MAPE | 0.1901<br>0.0020<br>0.1940 | 0.1918<br>0.0026<br>0.2147 | 0.1868<br>0.0031<br>0.2389 | 0.1943<br>0.0040<br>0.2668 | 0.2021<br>0.0182<br>0.5596 | -<br>MLE<br>MLE |
| (75,75,75)  |                        | Mean<br>MSE<br>MAPE | 0.1882<br>0.0014<br>0.1587 | 0.1899<br>0.0018<br>0.1784 | 0.1839<br>0.0023<br>0.2029 | 0.1919<br>0.0027<br>0.2206 | 0.2014<br>0.0168<br>0.5338 | -<br>MLE<br>MLE |
| (100,100,100)   |                        | Mean<br>MSE<br>MAPE | 0.1880<br>0.0010<br>0.1365 | 0.1881<br>0.0013<br>0.1543 | 0.1808<br>0.0019<br>0.1867 | 0.1887<br>0.0020<br>0.1934 | 0.2052<br>0.0157<br>0.5130 | -<br>MLE<br>MLE |